## GCE Physics - PH5

\begin{tabular}{|c|c|c|c|c|}
\hline \multicolumn{3}{|l|}{Question} \& Marking details \& Marks Available <br>
\hline \multirow[t]{12}{*}{1.} \& \multirow[t]{5}{*}{(a)

(b)} \& \& Correct $\alpha$ or $\beta$ absorber (1) \& <br>
\hline \& \& \& If drop after $\alpha$ absorber, then $\alpha$ present (1) (Alpha is stopped by paper - award 2 marks) \& <br>
\hline \& \& \& If further drop after $\beta$ absorber then $\beta$ present (1) \& <br>
\hline \& \& \& If (significant) count after $\beta$ absorber then $\gamma$ present or equivalent (1) \& <br>
\hline \& \& (i) \& $19 \times 10^{15}[\mathrm{~Bq}]$ \& 1 <br>
\hline \& \multirow{7}{*}{(b)} \& (ii) \& Use of $\lambda=\frac{\ln 2}{T_{1 / 2}}$ (1) e.g. 0.0271 per day or $3.13 \times 10^{-7} \mathrm{~s}^{-1} \quad$ (1) Or $A=\frac{A_{0}}{2^{x}}$ quoted \& <br>
\hline \& \& \& Or $A=\frac{A_{0}}{2^{x}}$ used \& <br>
\hline \& \& \& Substitutions of values (ignore wrong units or factors of ten slips) (1) Or $x=14.26$ \& <br>
\hline \& \& \& Correct answer $3.85 \times 10^{12}[\mathrm{~Bq}]$ (1) \& 4 <br>
\hline \& \& (iii) \& Attempt at using $A=\lambda N$ e.g. $76 \times 10^{15}=\lambda N(1)$ \& <br>
\hline \& \& \& $N=2.4 \times 10^{23}(1)$ \& 2 <br>
\hline \& \& \& Question 1 Total \& [11] <br>
\hline
\end{tabular}



| Question |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: |
| 3. | (a) | $Q=C V(1)$ |  |
|  |  | 212 [nC] (1) | 2 |
|  | (b) | Taking logs e.g. $\ln Q=\ln Q_{0}-\frac{t}{c R}(1)$ |  |
|  |  | $\text { Algebra } \quad \text { e.g. } R=-\frac{t}{\operatorname{cln} \frac{V}{V_{0}}}(1)$ |  |
|  |  | Substitution of correct values (1) <br> Answer $=1.36[\mathrm{M} \Omega](1)$ | 4 |
|  | (c) | $C=\frac{\varepsilon_{0} A}{d} \text { used e.g. rearranged (1) }$ |  |
|  |  | $\mathrm{A}=x^{2}($ or implied $) \rightarrow C=\frac{\varepsilon_{0} x^{2}}{d}$ first two marks (1) |  |
|  |  | Answer = 1.49 [m] (1) | 3 |
|  | (d) | Dielectric between plates | 1 |
|  |  | Question 3 total | [10] |



| Question |  |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: | :---: |
| 5. | (a) |  | The [induced] emf is proportional [or equal] to the rate of change [or cutting] of flux [linkage] or $\mathrm{d} B A N / \mathrm{d} t$ and terms defined <br> Nearly correct statements award 1 out of 2 marks e.g. <br> The emf is equal to the change of flux <br> The current is proportional to the rate of change of flux <br> The emf is proportional to the cutting of flux $B A N / t$ and terms defined <br> Wrong statements get 0 <br> The emf is equal/proportional to the flux linkage <br> The current is equal to the rate of change of flux | 2 |
|  |  |  | Lenz - the [induced] emf [or current] opposes [or tends to oppose etc.] the change [to which it is due] | 1 |
|  |  | (i) | Clockwise (1) any 1 of FLHR(must have correct direction), FRHR, right hand grip rule (1) | 2 |
|  |  | (ii) | Area increases $\checkmark$ at an increasing rate $\checkmark$ | 2 |
|  |  |  | or cutting of flux $\checkmark$ inside the loop $\checkmark$ <br> or $E=B l v \quad$ and $l$ is increasing $\checkmark$ |  |
|  |  | (iii) | $\begin{aligned} & V=\frac{B A N}{t} \text { and } t=\frac{20.1}{31}(=0.648 \mathrm{~s}) \quad \text { or } E=B l v \text { used }(1) \\ & A=\frac{1.8+2.9}{2} \times 20.1[=47.2] \quad \text { or mean } l=2.35[\mathrm{~m}](1) \end{aligned}$ |  |
|  |  |  | $I=\frac{V}{R}$ <br> Correct answer $\quad I=77[\mu \mathrm{~A}](1)$ | 4 |
|  |  |  | Question 5 Total | [11] |





| Question |  |  | Marking details | Marks <br> Available |
| :---: | :---: | :---: | :---: | :---: |
| 8. | (a) |  | Alternating current means an alternating $B$-field |  |
|  |  |  | [alternating] $B$-field transferred through core to secondary (1) |  |
|  |  |  | Changing flux inside the secondary coil [gives emf] (1) (accept flux cuts the secondary coil but not flux goes through secondary coil) | 3 |
|  | (b) |  | (needs design \& loss method) |  |
|  |  |  | Low resistance wires to reduce heat dissipation from wires (or equivalent) (1) |  |
|  |  |  | Laminated core to reduce eddy currents (1) |  |
|  |  |  | Suitable core alloy (or silicon steel etc.) to reduce magnetisation losses (or hysteresis or to reduce leakage flux/stray field etc.) (1) | 3 |
|  | (c) | (i) | $\omega=2 \pi f=24000\left[\mathrm{~s}^{-1}\right](1)$ |  |
|  |  |  | $\omega L=88.7$ [ $\Omega$ ] (1) |  |
|  |  |  | $\frac{1}{\omega c}=88.7[\Omega] \text { (1) }$ | 3 |
|  |  | (ii) | Reactances are the same (accept impedances) <br> (this can be stated regardless of a wrong answer to (i)) | 1 |
|  |  | (iii) | Answer $=6.5[\mathrm{~mA}]$ (allow ecf if full method followed through) | 1 |
|  |  |  | (i.e. using $Z=\sqrt{\left(\omega L-\frac{1}{\omega C}\right)^{2}+R^{2} \text { etc.) }}$ |  |

\begin{tabular}{|c|c|c|c|c|}
\hline \multicolumn{3}{|l|}{Question} \& Marking details \& Marks Available <br>
\hline \multirow[t]{10}{*}{8.} \& \multirow{10}{*}{(d)} \& \multirow[t]{4}{*}{(iv)

(i)} \& Ignore capacitance (or $\omega L-\frac{1}{\omega C}$ attempted) (1) \& <br>
\hline \& \& \& Correct calculation for impedance e.g.. $\sqrt{887^{2}+2200^{2}}$ (1) \& <br>

\hline \& \& \& $$
\text { Answer }=\frac{14.4}{2370}=6.1[\mathrm{~mA}](1)
$$ \& 3 <br>

\hline \& \& \& Attempt at an explanation at low and high frequency (1) \& <br>
\hline \& \& \& Correct variation of $X_{C}$ with frequency (i.e. large at low frequency or low at high frequency) (1) \& <br>
\hline \& \& \& Correct division of pd with respect to frequency (e.g. at high frequency $R \gg X_{C}$ so $V_{\text {OUT }}$ is large or the opposite at low frequency) (1) \& 3 <br>
\hline \& \& (ii) \& Phasor diagram drawn or implied (1) V \& <br>
\hline \& \& \& $X_{C}=R$ or $V_{C}=V_{R}$ either derived or quoted (implies diagram correct) (1) \& <br>
\hline \& \& \& Answer $=154[\mathrm{~Hz}]$ (1) \& <br>
\hline \& \& \& Question 8 Total \& [20] <br>
\hline
\end{tabular}

| Question |  |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: | :---: |
| 9. | (a) | (i)(I) |  | 2 |
|  |  | (II) | Prograde and motion on epicycle and deferent in same direction - or equivalent | 1 |
|  |  | (III) <br> (ii) <br> (I) | Brightness or size <br> Either $\frac{2 \pi}{T_{E / J}} \Delta t(1)$ represents angle swept out by Earth/Jupiter in time <br> $\Delta t$ (1) <br> OR $\frac{\Delta t}{T_{E / J}}$ (1) represents fraction of a cycle swept out by Earth/Jupiter in time $\Delta t$ Earth sweeps out extra angle $2 \pi$ or one extra revolution (1) | $\begin{aligned} & 1 \\ & 2 \end{aligned}$ |
|  |  | (II) | $\begin{aligned} & \frac{1.092}{1}-\frac{1.092}{T_{J}}=1(1) \\ & 1.092 T_{J}-1.092=1 T_{J} \\ & T_{J}=11.9 \text { [years] (1) } \end{aligned}$ | 2 |
|  | (b) | (i) | Nesting of: sphere of mercury / solid / sphere of Venus/solid (1) <br> Didn't give quite correct orbital radii (1) | 2 |


| Question |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: |
| (c) <br> (d) | (ii) | Mention of Plato or Pythagoras (1) |  |
|  |  | Nature based on mathematics (or equivalent) (1) | 2 |
|  | (i) | Path of body acted on by central force [towards S] Accept path of planet. (1) |  |
|  |  | [Central] force applied at [just] these points (1) | 2 |
|  | (ii) | Equal areas in equal times OR area swept out proportional to time | 1 |
|  | (i) | Use of or by implication : (1) $\frac{v^{2}}{r g_{\text {surf }}} \operatorname{or} \frac{r \omega^{2}}{g_{\text {surf }}}=2.78 \times 10^{-4}(1)$ | 2 |
|  | (ii) | Attempt to evaluate $\left(\frac{r_{E}}{r_{M O}}\right)^{2}$ $=2.75 \times 10^{-4}(1)$ | 2 |
|  | (iii) | Either: spherically symmetric OR behaves as if all at centre | 1 |
|  |  | Question total | [20] |


| Question |  |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: | :---: |
| 10. | (a) | (i) | Diameter[accept width/thickness do not accept radius/area] $\rightarrow$ micrometer/digital calliper [accept vernier calipers but not vernier only] (1) <br> Original [accept natural] length $\rightarrow$ metre rule (1) | 2 |
|  |  | (ii) | Take (one set of) $F$ and $e$ from graph or Measure gradient $[$ or $=F / \Delta x]$ Accept gradient $=E A / l(1)$ <br> Use value of $\pi d^{2} / 4$ or $\pi r^{2}$ [explanation of how $A$ is calculated required - can be awarded from (i)] (1) |  |
|  |  |  | Insert in relevant equations <br> (1) $Y=\frac{F l_{0}}{A \Delta x}$ or $Y=\operatorname{grad} \times \frac{l_{0}}{A}$ etc. | 3 |
|  | (b) | (i) | $\left[e_{\text {iron }}\right]=\frac{F l_{0}}{A E_{\text {iron }}}\left[\text { must show } \frac{F l_{0}}{A}\right]$ | 1 |
|  |  | (ii) | Attempt at $e_{\text {brass }}+e_{\text {iron }}$ (1) |  |
|  |  |  | Correct manipulation/algebra (1) | 2 |
|  |  | (iii) | CSA calculated: $7.9 \times 10^{-7}\left[\mathrm{~m}^{2}\right]$ (1) |  |
|  |  |  | Substitution (ecf on CSA) (1) |  |
|  |  |  | $W=0.042[\mathrm{~J}]$ (1) $[-1$ for slip in power of $10 ;-1$ for use of diameter instead of radius] |  |
|  |  | (iv) | 1.8 mm UNIT mark | 1 |


| Question |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: |
| (c) | (v) | Greater extension by brass [or smallest extension by iron] (1) | 4 |
|  |  | $e \sim 1 / E$ (1) [link Young modulus to extension] |  |
|  |  | All other factors same for both wires (1) |  |
|  |  | Ratio 2:1 ( $1.2 \mathrm{~mm}: 0.6 \mathrm{~mm}$ ) (1) [Full marks may be obtained by calculation only]. |  |
|  | (i) | Melamine formaldehyde $\rightarrow$ thermosetting (1) |  |
|  |  | Low density polyethylene $\rightarrow$ thermoplastic (1) | 2 |
|  | (ii) | Melamine brittle - low max strain (1) |  |
|  |  | or polythene not brittle - high max strain |  |
|  |  | Melamine stiffer - higher Young modulus (1) | 2 |
|  |  | or polythene less stiff - lower Young modulus |  |
|  |  | [or accept low strain for high stress as explanation for stiffness of material] |  |
|  |  | Question total | [20] |



| Question |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: |
| (b) | (i) | $Z=$ Density x velocity [of ultrasound in the material] Must be in words as equation is given Do not accept speed of light for velocity | 1 |
|  | (ii) | $Z_{1}=442$ and $Z_{2}=1700 \times 10$ |  |
|  |  | $f=\operatorname{approx} 1 / 0.995(1)$ | 2 |
|  | (iii) | Almost all ultrasound reflected/ none able to enter the body (1) |  |
|  |  | Need for a coupling gel/medium (1) | 2 |
| (c) | (i) | Exposure: amount of radiation incident on the body (1) Do not accept: 'total radiation exposed to' as it is a rewrite of the question. | 2 |
|  |  | absorbed dose: energy per unit mass absorbed by body (1) |  |
|  | (ii) | Dose equivalent $=$ dose x quality factor (1) Do not accept in terms of units |  |
|  |  | Quality factor depends on ionization or alpha $Q=20$ and gamma $Q=1(1)$ | 3 |
|  |  | Greater for alpha than gamma (1) |  |
|  |  | Question total | [20] |


| Question |  |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: | :---: |
| 12. | (a) | (i) | Any 2 x (2) from <br> Easily controllable Accept: no chain reaction (1) <br> Because can switch off protons/hydrogen (1) <br> OR <br> No radioactive by-products or products are alpha particles (1) <br> Any good relevant detail e.g. no storage costs for thousands of years <br> Or alpha particles easily contained etc. (1) <br> OR <br> Fuel cheaper than fuel for fission (1) <br> Detail e.g. per MJ output, H from the sea, no isotope enrichment needed, selling the He would help pay for the fuel (1) <br> OR <br> Fuel supplies would last longer than for fission (1) <br> Detail: sensible remarks about $U$ and $H$ (1) <br> $30000000 \times 300 \mathrm{keV}$ (in whatever units) (1) <br> Conversion so that answer and reaction energy in the same units (i.e. 9 million MeV or equivalent e.g. $2.74 \times 10^{-12}$ and $1.44 \times 10^{-6} \mathrm{~J}$ ) <br> (1) | 4 |
|  |  | (iii) | Comment implying far less energy out than in (1) $7 \times 1.66 \times 10^{-27} \text { seen (1) }$ | 3 |
|  |  | (iv) | Answer $\left[10^{16} / 7 \mathrm{u}\right]=8.6 \times 10^{41}(1)$ <br> Answer (iii) x 17.1 MeV (or its J equivalent $2.74 \times 10^{-12}$ ) (1) Tolerate slips in powers of 10 ; answer mark will be lost. <br> previous answer / $5 \times 10^{20}$ (regardless of mixed units) (1) | 2 |
|  |  |  |  | 3 |


| Question |  | Marking details | Marks Available |
| :---: | :---: | :---: | :---: |
| (b) | (i) | Area $=20 \mathrm{~mm} \times 20 \mathrm{~mm}$ or implied (1) Including side-faces loses the mark. <br> Temperature difference $=150\left[{ }^{\circ} \mathrm{C}\right](1)$ <br> Heat $=2040$ [W] (1) <br> ecf on $A$, provided not a volume instead of an area | 3 |
|  | (ii) <br> (iii) | Work is done on the gas (1) <br> Internal energy of the gas increases (no heat not required) (1) Freestanding mark i.e. accept if wrongly deduced, but only if link with temperature rise made. <br> Efficiency $=1-\frac{T_{2}}{T_{1}} \quad$ accept $\frac{Q_{1}-Q_{2}}{Q_{1}}$ or $1-\frac{Q_{2}}{Q_{1}}(1)$ <br> $T_{1}$ is larger or $\frac{T_{2}}{T_{1}}$ is smaller <br> $Q_{1}$ is larger or $\frac{\frac{T_{1}}{Q_{2}}}{Q_{1}}$ is smaller but these need an explanation e.g. <br> because temperature is higher. If done by putting temperatures into formula, they must be in K. (1) <br> Efficiency is greater in equation (not an independent mark i.e. valid earlier argument needed, ignoring ${ }^{\circ} \mathrm{C}$ instead of K ) (1) <br> Question total | 2 <br> 3 <br> [20] |

